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UNCLASSIFIED SECURITY CLASSIFICATION OF THIS PAGE (When Date & READ INSTRUCTIONS / REPORT DOCUMENTATION PAGE BEFORE COMPLETING FORM . REPORT NUMBER 2. GOVT ACCESSION NO. 3. RECIPIENT'S CATALOG NUMBER AD94 443 NADC-80181- E-60 TITLE (and Subtitle) TYPE OF REBORT A PERIOD COVERED Maritime Patrol Aircraft (MPA) Concept Final Report. Porterior Allison PD371-47 Oct 78 - Feb 79 PERFORMING ORG. REPORT NUMBER Advanced Turboprop -EDR-9777A AUTHOR(a) S. CONTRACT OR GRANT NUMBER(s) P. /Stolp / N62269-78-C-0415 PERFORMING ORGANIZATION NAME AND ADDRESS PROGRAM ELEMENT, PROJECT, TASK AREA & WORK UNIT NUMBERS Detroit Diesel Allison 65152N Division of General Motors Corporation, Box 894 A03P-03PA/001E/7W0880/001 Indianapolis, IN 46206 Work Unit XM201 11. CONTROLLING OFFICE NAME AND ADDRESS 12. REPORT DATE. Naval Air Development Center Warminster, PA 18974 14. MONITORING AGENCY NAME & ADDRESS(II different from Controlling Office) 18. SECURITY CLASS. (of this report) UNCLASSIFIED 15a. DECLASSIFICATION/DOWNGRADING 16. DISTRIBUTION STATEMENT (of this Report) APPROVED FOR PUBLIC RELEASE; DISTRIBUTION UNLIMITED 17. DISTRIBUTION STATEMENT (of the electroct entered in Block 20, If different from Report) 18. SUPPLEMENTARY NOTES 19. KEY WORDS (Continue on reverse side if necessary and identify by block number) Turbofan Engine Aircraft Propulsion Derivative Engine Turboshaft Engine Maritime Patrol Aircraft Turboprop Engine 20. ABSTRACT (Continue on reverse side if necessary and identify by block number) This study developed data on Detroit Diesel Allison (DDA) common core derivative engines for use in Maritime Patrol Aircraft (MPA) concept formulation studies. The study included the screening of potential DDA turboprop/

This study developed data on Detroit Diesel Allison (DDA) common core derivative engines for use in Maritime Patrol Aircraft (MPA) concept formulation studies. The study included the screening of potential DDA turboprop/turboshaft engines and the preparation of technical and planning information on three of the most promising engine candidates plus an all new engine. Screening of DDA derivative candidates was performed utilizing an analytical MPA model using synthesized mission profiles to rank the candidates in terms

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wof fuel consumption, weight, cost and complexity. The three turboprop engines selected for further study were as follows: a derivative of the unity size T701-AD-700 shaft power engine with rematched turbine (PD 370-37), an advanced T701 turboprop derivative with 25:1 overall pressure ratio and a scaled ATEGG demonstrated compressor (FD 370-40), an advanced T701 turboprop derivative with 17.7:1 overall pressure ratio and a scaled ATEGG demonstrated compressor (PD 370-41). Data is also presented on a new advanced turboprop engine with 30:1 overall pressure ratio which incorporates compressor, combustor, turbine, and cooling technology now under development and demonstration at DDA. The documentation consists of six seperate reports prepared in the following manner. One report summarizes the engine screening analysis and describes the approach to, and the conclusions of the study. A separate report for each of the three derivative engines and for the new turboprop present estimates of performance, weight, and dimensional data. The engineering budgetary estimates of the development, acquisition, and service costs for each of the four engines are presented in a separate report.

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REVISIONS

Letter	Page	Revision
A	4	All weights
A	6	All weights
A	10	Additional matrix points at 0 and 25,000 feet
A	13	Additional performance
A	18	Additional performance
A	23	Additional performance
A	28	Additional performance



I. INTRODUCTION

This report presents estimates of performance, weight, and dimensional data for the PD 370-42 turboprop engine. The PD 370-42 is an advanced turboprop engine with 30:1 overall pressure ratio. It incorporates compressor, combustor, turbine, and cooling techniques now under development and demonstration at DDA. The technologies represent the highest levels that can be offered for IOC's circa 1990's. The engine is in the 9,000 to 10,000 SHP class, but scaling data is included to provide for studies down to 6,000 and up to 12,000 SHP. The data is submitted for use in preliminary design type studies in the evaluation of turboprop systems.

The reduction gearbox for speed reduction to the prop-fan is a new simplified design, compared to the DDA T56 series of gearboxes. The new design is based upon a study into the reliability and maintenance cost history of past turbo-prop systems, and follows the recommendations of that study for a gearbox with high reliability, easy maintainability, and low maintenance costs.



II. ENGINE DESCRIPTION

The Model PD 370-42 is an axial flow engine, having a single spool core and a free power turbine connected by shafting, and supporting structure to an offset reduction gear assembly. The general arrangement and external features of the engine are shown in Figure II-1, with principle physical characteristics listed in Table II-I. Output speed of the engine is constant at 12,860 RPM. The reduction gearbox shown in Figure II-1 has an overall gear ratio of 9.52:1, providing a propfan speed of 1351 rpm at 12,860 engine rpm. Parametric weight data is shown in Section III so that other propfan rotational speeds, and gear ratios can be analyzed. An aircraft accessory drive pad is provided on the back of the gearbox to drive an aircraft mounted accessory drive box. Power available at this pad is 500 HP at 8000 rpm. The primary engine mounts are on the gearbox with a hang mount at the rear of the engine. Engine accessories are driven by a bevel drive from the high pressure spool. The control system is integral with the propfan and is digital electronic. The oil system is integral to the engine and also supplies the propfan and reduction gearbox, but is separately filtered and monitored to isolate fault detection in each of these major modules. Engine torque is measured hydraulically from the gear thrust of the power train idler gears in the reduction gearbox.

The gearbox is shown offset, based upon DDA's experience with large turboprop engines. It is offset-up to be consistent with current studies showing a preference to under-the-wing engine mounting. It can also be supplied in the offset-down position.

Performance ratings, sea level static, are listed in Table II-II.

For preliminary design studies, the PD 370-42 engine configuration can be scaled to other power ratings. Scaling information is included for dimensions, weight, and performance.

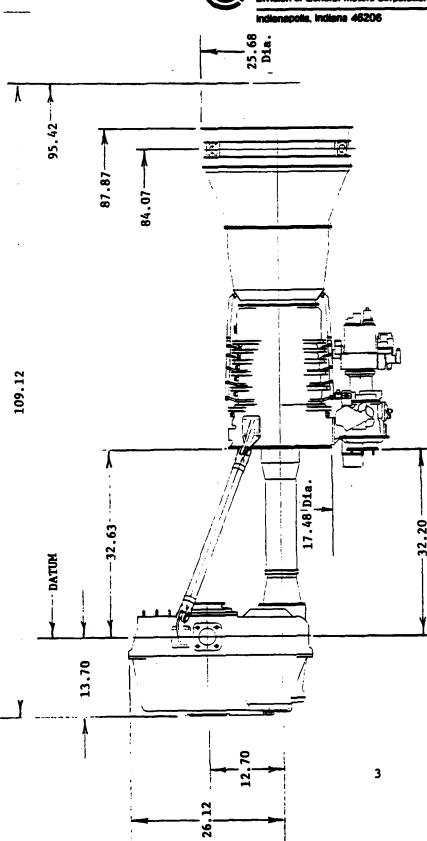


Figure II-1. PD370-42 General Arrangement.



TABLE II-I

PD 370-42 PHYSICAL CHARACTERISTICS

Length (in)

(Includes Gearbox)

109.12

•	
Max. Engine Diameter (in)	25.68
Max. Gearbox Offset, upward (in)	26.12
Dry Weight, 1bs	
Engine	886 299 SEC
Gearbox, including interconnecting struts and shaft	585 4 68
Total	147/ 1367

For scaling dimensions the following formulae may be used for SHP's up to 12,000 and down to 6,000, and for other reduction gear ratios than 9.52:1.

Engine

Axial dimensions = Base dim.
$$x \left(\frac{SHP}{9,610} \right)^{0.4}$$

Diameters = Base dia. $x \left(\frac{SHP}{9,610} \right)^{0.5}$

Reduction Gearbox

Dimensions = Base dim.
$$\times \left(\frac{SHP}{9,610}\right)^{0.5} \times \left(\frac{GR}{9.52}\right)^{0.33}$$

Shaft length remains unchanged.



TABLE II-II

PD370-42 PERFORMANCE SUMMARY

Sea Level, 0 kts

	Star	ndard Day	Hot Day, 89.8°F			
	SHP	SFC	F _N	SHP	SFC	F _N
Take-Off	9,610	0.348	827	7,924	0.363	645
Max. Continuous	7,302	0.363	604	5,989	0.381	474

III. WEIGHTS

The weight of the basic 9,610 SHP engine, gearbox, and the interconnecting struts and shaft are given in Table III-I. The gearbox weight is based upon a gear ratio of 9.52:1 which provides a propfan speed of 1351 rpm.

TABLE III-I

PD 370-42 WEIGHTS

	Dry	Wet*	Installed
Basic Engine, 1bs	886	907	907
Gearbox, lbs	557	597	597
Interconnecting Struts and Shaft, 1bs	28	28	28
Total, 1bs	1471	1532	1532

^{*} Includes total amount of oil required for engine and gearbox operation.

For scaling weights to engine sizes up to 12,000 and down to 6,000 SHP, and for other reduction gear ratios, the following formulae may be used:

Engine weight = 886 x
$$\left(\frac{HP}{9,610}\right)$$
 1.01

Gearbox weight = 557 x
$$\left(\frac{HP}{9,610}\right)^{1.5}$$
 x $\left(\frac{GR}{9.52}\right)^{0.4}$

Interconnecting strut and shaft weight = 5.1% of dry gearbox weight

Indianapolis, Indiana 46206

IV. STEADY STATE PERFORMANCE

Steady state performance data is tabulated in this section for all points shown in Figure IV-1. Basic engine data is shown for the following assumptions:

- o Uninstalled engine
- o ICAO standard atmosphere except for takeoff which in addition includes an ambient temperature of 89.8°F at standard atmosphere
- o 100% inlet recovery
- o Zero accessory horsepower extraction
- o Zero customer bleed extraction
- o Zero losses due to reduction gear
- o Fuel heating value 18,400 Btu/lb
- o Estimated average engine performance No SHP or fuel flow guarantee factors

Sensitivity data is provided for each point so that bleed and duct losses may be estimated as required.

Nomenclature

Nomenclature used in the tabulation of performance is as follows:

MACH	Mach number
SHP	Shaft horsepower
SFC	Specific fuel consumption, lbs/hr/hp
WF .	Engine fuel flow, lbs/hr
FN	Net jet thrust, 1bs (jet gross thrust - ram drag)
ESHP	Equivalent shaft horsepower (energy in jet stream converted ideally to horsepower and added to SHP)
WCIN	Total inlet corrected airflow, $\sqrt[4]{\theta_1}/\xi_1$
	where: $\theta_1 = \text{Engine inlet total temp, }^{O}R$
	518.688



S₁ = Engine inlet total pressure, psi 14.696

TNOZ Jet nozzle total temperature, OR

PNOZ Jet nozzle total pressure, psi

RC Compressor pressure ratio

BOT Burner outlet temperature, OR

NO Point number

Sensitivity Data

Bleed:

SHP, with bleed = SHP, no bleed - (DEL SHP) (% bleed)

WF, with bleed = WF, no bleed - (DEL WF) (Z bleed)

FN, with bleed = FN, no bleed - (DEL FN) (% bleed)

Inlet Recovery:

7 = Total pressure actual/Total pressure ideal

SHP, with recovery = SHP, ideal recovery - (DEL SHP)(1 - η_R)(100)

WF, with recovery = WF, ideal recovery (\mathcal{T}_R)

FN, with recovery = FN, ideal recovery - (DEL FN) $(1 - \eta_R)$ (100)

Jet Nozzle Duct Loss:

To estimate thrust loss due to additional duct loss prior to the jet nozzle, use the following equation:

FN, with loss = FN, without loss - FN, without loss (K) (ΔP)

where.

- o K is obtained for each point from sensitivity data
- o ΔP = PTOT, no loss PTOT, total loss
 PTOT, no loss

Reduction Gear Loss:

Reduction gear is 99 percent efficient.

Accessory Drive Losses:

Accessory drive power extraction is directly from the accessory drive pad on the reduction gearbox. Reduce SHP to prop-fan by amount of accessory power extraction at each point.

Scale Effect on SHP and SFC:

The engine performance is scaleable for purposes of studying other engine sizes. However, component performance will vary, dependent upon the amount of scale. A correction to scale factor for SHP and SFC was formulated for component performance changes and the effects on SHP, SFC, and FN are as follows:

Scaled SHP = Unscaled SHP X $\left(1-\frac{A}{100}\right)$ X Scale Factor

Scaled FN = Unscaled FN X Scale Factor

Scaled SFC = Unscaled SFC X $\left(1 + \frac{B}{100}\right)$

where:

Scale Factor = Desired Rating (limited from 0.6 to 1.25) Unity Rating

A = Sizing effect on SHP

= 11.94 x Scale factor - 3.80 x (Scale factor)² - 8.14

B = Sizing effect on SFC

= 2.98 x (Scale factor) 2 - 9.46 x Scale factor + 6.48

Nozzle Throat Area

The effective nozzle throat area is constant for all conditions at 263.9 in 2.

Indianapolis, Indiana 46206

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닒	.2	×
MACH Number	.1	×
	0	×
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Standard and Hot Day; Takeoff and Maximum Continuous

Standard Day; Maximum Climb, Maximum Continuous and Part Power to Idle

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Altitude	$(\text{Ft} \times 10^{-3})$	0	5	10	15	20	25	30	35	07	45

Figure IV-1. Matrix of flight conditions for performance data

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SENSITIVITY DATA FOR BLEED, INLET RECOVERY, AND EXHAUST DUCT LOSS

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SENSITIVITY DATA FOR BLEED, INLET RECOVERY, AND EXHAUST DUCT LOSS 20000 FEET ALTITUDE

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DETROIT DIESEL ALLISON DIVISION

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PD370-42 TURBOPROP

SENSITIVITY DATA FOR BLEED, INLET RECOVERY, AND EXHAUST DUCT LOSS

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